

# Local Dynamics at the Apex of an Astropause: Insights from 3D Resistive MHD Solutions

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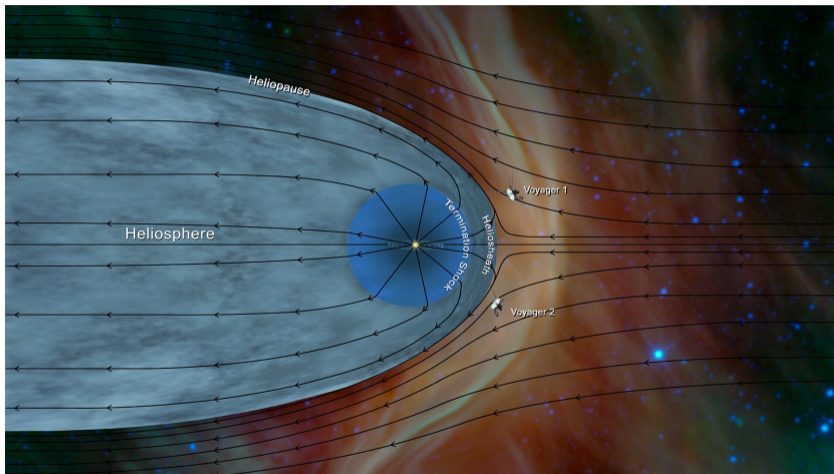
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# Motivation



Credits: NASA JST

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# Magnetohydrodynamics

- Describes the dynamics of a conducting fluid in the presence of electromagnetic fields.

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

$$\rho \frac{\partial \mathbf{v}}{\partial t} + \rho \mathbf{v} \cdot \nabla \mathbf{v} = -\nabla p + (\nabla \times \mathbf{B}) \times \mathbf{B}$$

$$\frac{\partial \mathbf{B}}{\partial t} = \nabla \times (\mathbf{v} \times \mathbf{B}) - \nabla \times (\eta \nabla \times \mathbf{B})$$

$$\nabla \cdot \mathbf{B} = 0$$

- It is useful to express the equations in terms of dimensionless quantities. Independent variables and differential operators:

$$\bar{l} = l/l_0, \quad \bar{t} = t/t_0 \quad \Rightarrow \quad \bar{\nabla} = l_0 \nabla, \quad \partial/\partial \bar{t} = t_0 \partial/\partial t$$

- Dimensionless dependent variables:

$$\bar{\rho} = \rho/\rho_0 \quad \bar{\mathbf{v}} = \mathbf{v}/v_0 \quad \bar{p} = p/(\rho_0 v_0^2) \quad \bar{\mathbf{B}} = \mathbf{B}/B_0$$

# Linear Flows

- Fields close to the null points can be Taylor expanded.
- Assumption: The velocity null and the magnetic null coincides.
- Taylor Series for a scalar:

$$f(x) = f(a) + \frac{f'(a)}{1!}(x-a) + \frac{f''(a)}{2!}(x-a)^2 + \dots$$

- Taylor Expanding fields:

$$\mathbf{v} = \mathcal{V} \cdot \mathbf{r}$$

$$\mathbf{B} = \mathcal{B} \cdot \mathbf{r}$$

$$p = \mathbf{r}^T \cdot \mathcal{P} \cdot \mathbf{r} + p_0$$

where

$$\mathbf{r} = (x \quad y \quad z)^T$$

$$\mathcal{V}_{ij} = \frac{\partial v_i}{\partial x_j} = \begin{pmatrix} V_{11} & V_{12} & V_{13} \\ V_{21} & V_{22} & V_{23} \\ V_{31} & V_{32} & V_{33} \end{pmatrix}$$

$$\mathcal{B}_{ij} = \begin{pmatrix} 1 & \frac{(q-j_{\parallel})}{2} & 0 \\ \frac{(q+j_{\parallel})}{2} & b & 0 \\ 0 & j_{\perp} & -(b+1) \end{pmatrix}$$

$$\mathcal{P}_{ij} = \frac{\partial^2 p}{\partial x_i \partial x_j}$$

# 3D Linear Dynamical System

- Equations of the form  $\dot{\mathbf{v}} = \mathcal{V} \cdot \mathbf{r}$ , where  $\mathcal{V}$  has three eigenvalues  $\lambda_1$ ,  $\lambda_2$  and  $\lambda_3$ .
- Saddle Points
  - Not all eigenvalues have real parts with the same sign.
  - Topological skeleton has two components: Fan plane and the Spine line.
  - Fields moving towards the null point: Stable subspace, and fields moving away from the null: Unstable subspace.
  - The null is radial if all eigenvalues are real, and is a spiral if two of the eigenvalues are complex conjugates.

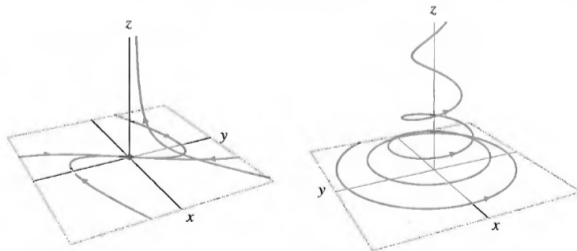


Figure: (a) Radial null and (b) Spiral null

# 3D Magnetic Field Structure

- The magnetic field is given by  $\mathbf{B} = \mathcal{B} \cdot \mathbf{r}$ , where the matrix  $\mathcal{B}$  is prescribed as:

$$\mathcal{B} = \begin{pmatrix} 1 & \frac{(q-j_{\parallel})}{2} & 0 \\ \frac{(q+j_{\parallel})}{2} & b & 0 \\ 0 & j_{\perp} & -(b+1) \end{pmatrix} \quad \mathbf{j} = \begin{pmatrix} j_{\perp} \\ 0 \\ j_{\parallel} \end{pmatrix}$$

- To determine the topological structure, we need to compute the eigenvalues.

$$\lambda_{B_{1,2}} = \frac{1}{2}(b+1) \pm \frac{1}{2}\sqrt{j_c^2 - j_{\parallel}^2} \quad \lambda_{B_3} = -(b+1) \quad \begin{array}{l} b \geq -1 \\ (b+1)^2 \geq j_c^2 - j_{\parallel}^2 \\ j_c^2 = (b-1)^2 + q^2 \end{array}$$

- Note that as  $\mathcal{B}$  is traceless, the magnetic field is always a saddle point.

- Solved the stationary MHD equations locally for constant resistivity.
- Flow is considered to be incompressible ( $\nabla \cdot \mathbf{v} = 0$ )

- Stationary MHD equations:

$$\mathcal{V}^2 - \mathcal{V}^T \mathcal{V} = \mathcal{B}^2 - \mathcal{B}^T \mathcal{B} \quad (1)$$

$$\text{tr}(\mathcal{V}) = 0 \quad (2)$$

$$\mathcal{V}\mathcal{B} - \mathcal{B}\mathcal{V} = 0 \quad (3)$$

$$\text{tr}(\mathcal{B}) = 0 \quad (4)$$

- The pressure is given by:

$$\mathcal{P} = \mathcal{B}^2 - \mathcal{B}^T \mathcal{B} - \mathcal{V}^2 \quad (5)$$

- (2) and (3)  $\Rightarrow$

$$\mathcal{V}_{12} = (j_{\parallel} - q)(\mathcal{V}_{11} - \mathcal{V}_{22}) / [2(b - 1)], \quad (A1)$$

$$\mathcal{V}_{13} = 0, \quad (A2)$$

$$\mathcal{V}_{21} = (j_{\parallel} + q)(\mathcal{V}_{22} - \mathcal{V}_{11}) / [2(b - 1)], \quad (A3)$$

$$\mathcal{V}_{23} = 0, \quad (A4)$$

$$\mathcal{V}_{31} = \frac{6j_{\perp}(j_{\parallel} + q)(\mathcal{V}_{22} - b\mathcal{V}_{11})}{(b - 1)(j_{\parallel}^2 + 8b^2 + 20b + 8 - q^2)}, \quad (A5)$$

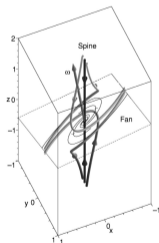
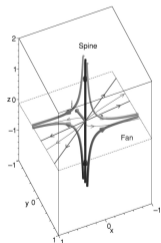
$$\mathcal{V}_{32} = j_{\perp} \{ [4(b^2 + b - 2) - j_{\parallel}^2 + q^2] \mathcal{V}_{11} + [8(b^2 + b - 2) + j_{\parallel}^2 - q^2] \mathcal{V}_{22} \} / (b - 1)(j_{\parallel}^2 + 8b^2 + 20b + 8 - q^2), \quad (A6)$$

$$\mathcal{V}_{33} = -(\mathcal{V}_{11} + \mathcal{V}_{22}). \quad (A7)$$



- The momentum equation (1) is a skew-symmetric matrix, i.e. three equations for 2 parameters.
  - Field-Aligned (FA) flows:

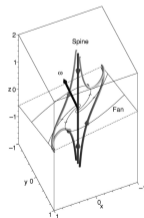
$$V_{11} = \pm 1 \quad V_{22} = \pm b \quad \Rightarrow \mathcal{V} = \pm \mathcal{B}$$



- Spiral field-crossing (SFC) flows:

$$V_{11} = \pm(1 - b^2 + S^2)/(2S) \quad S^2 = (j_{\parallel}^2 - j_{\perp}^2)/3$$

$$V_{22} = \pm(b^2 - 1 + S^2)/(2S)$$



- The fan and spine for both fields always coincide.

# MHD Equations Revisited

Full MHD equations:

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = -\nabla p + (\nabla \times \mathbf{B}) \times \mathbf{B}$$

$$\nabla \cdot \mathbf{v} = 0$$

$$\nabla \times \mathbf{B} = \mathbf{j}$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\mathbf{E} + \mathbf{v} \times \mathbf{B} = \eta \mathbf{j}$$

Stationary case for the Linearized fields:

$$\mathcal{V}^2 - \mathcal{V}^{T2} = \mathcal{B}^2 - \mathcal{B}^{T2} \quad (6)$$

$$\text{tr}(\mathcal{V}) = 0 \quad (7)$$

$$\nabla \times \mathbf{E} = 0 \quad (8)$$

$$\mathbf{E} + \mathbf{v} \times \mathbf{B} = \eta \mathbf{j} \quad (9)$$

$$\text{tr}(\mathcal{B}) = 0 \quad (10)$$

The pressure can be calculated as:

$$\mathcal{P} = \mathcal{B}^2 - \mathcal{B}^T \mathcal{B} - \mathcal{V}^2 \quad (11)$$

- The Electric field can be written as a gradient of a scalar function.

$$\nabla \times \mathbf{E} = 0 \quad \implies \quad \mathbf{E} = -\nabla\phi \quad (12)$$

- The Ohm's law is a set of three equations, one for each component.

$$-\frac{\partial\phi(x, y, z)}{\partial x} + v_y B_z - v_z B_y = \eta(x, y, z)j_{\perp} \quad (13a)$$

$$-\frac{\partial\phi(x, y, z)}{\partial y} + v_z B_x - v_x B_z = 0 \quad (13b)$$

$$-\frac{\partial\phi(x, y, z)}{\partial z} + v_x B_y - v_y B_x = \eta(x, y, z)j_{\parallel} \quad (13c)$$

- The uniqueness of  $\eta(x, y, z)$ , the condition of incompressibility, and the momentum equation provides us with 7 constraints for 9 velocity matrix elements.

- We choose the independent parameters to be  $V_{11}$  and  $V_{13}$ .
- The velocity matrix can now be expressed in terms of the magnetic field parameters and two free parameters, namely  $V_{11}$  and  $V_{13}$ .

$$\mathcal{V} = \mathcal{V}(V_{11}, V_{13}, b, q, j_{\parallel}, j_{\perp}) \quad (14)$$

- The solutions can be categorized into four classes.

	$V_{11}$	$V_{13}$
class I	0	0
class II	1	0
class III	0	1
class IV	1	1

$$\mathcal{V}_1(V_{11}, b, q, j_{\parallel}, j_{\perp}) = \begin{pmatrix} \frac{V_{11}}{(q+j_{\parallel})} & \frac{(q-j_{\parallel})}{2} & 0 \\ 0 & \frac{3j_{\parallel}(1+b-V_{11})+q(-1+b+V_{11})}{(q+3j_{\parallel})} & 0 \\ 0 & j_{\perp} & \frac{-3(1+b)j_{\parallel}-q(-1+b+2V_{11})}{(q+3j_{\parallel})} \end{pmatrix} \quad (15)$$

$$\mathcal{V}_2(V_{11}, b, q, j_{\parallel}, j_{\perp}) = \begin{pmatrix} \frac{V_{11}}{(q+j_{\parallel})} & -\frac{(q-j_{\parallel})}{2} & 0 \\ -\frac{(q+j_{\parallel})}{2} & \frac{-3j_{\parallel}(1+b+V_{11})+q(1-b+V_{11})}{(q+3j_{\parallel})} & 0 \\ 0 & -j_{\perp} & \frac{3(1+b)j_{\parallel}+q(-1+b-2V_{11})}{(q+3j_{\parallel})} \end{pmatrix} \quad (16)$$

- They have a similar form as the magnetic field.

$$\mathcal{B} = \begin{pmatrix} 1 & \frac{(q-j_{\parallel})}{2} & 0 \\ \frac{(q+j_{\parallel})}{2} & b & 0 \\ 0 & j_{\perp} & -(b+1) \end{pmatrix} \quad (17)$$

- We consider the special case where  $V_{11} = 1$  or  $V_{11} = -1$ .

$$\mathcal{V}_1(1, 0) = -\mathcal{V}_2(-1, 0) = \mathcal{B} \quad (18)$$

$$\mathcal{V}_1(-1, 0) = -\mathcal{V}_2(1, 0) = \begin{pmatrix} -1 & \frac{(q-j_{\parallel})}{2} & 0 \\ \frac{(q+j_{\parallel})}{2} & -2 + b + \frac{12j_{\parallel}}{q+3j_{\parallel}} & 0 \\ 0 & j_{\perp} & 3 - b - \frac{12j_{\parallel}}{q+3j_{\parallel}} \end{pmatrix} \quad (19)$$

- If we fix  $c_1 = c_2 = 0$  for our ansatz, we get constant resistivity.

$$\eta(x, y, z) = c_3$$

## Example: Radial Null

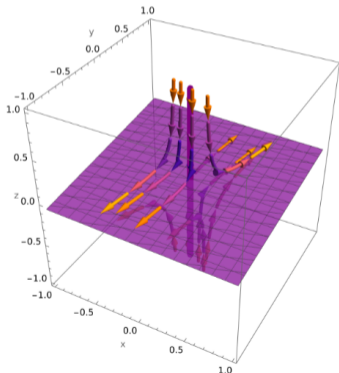
- We investigate the dependence of solutions  $\mathcal{V}_1$  on the free parameter  $V_{11}$  for specific magnetic field configurations.
- For the first example, we fix the magnetic field parameters to be  $b = 5, q = 3, j_{\perp} = 1$  and  $j_{\parallel} = 1$ . This configuration corresponds to a radial magnetic null.

$$B = \begin{pmatrix} 1 & 1 & 0 \\ 2 & 5 & 0 \\ 0 & 1 & -6 \end{pmatrix}$$

$$\lambda_{B_1} = 5.44949$$

$$\lambda_{B_2} = 0.55051$$

$$\lambda_{B_3} = -6.0$$



## Example: Radial Null

- the Velocity field takes the simplified form

$$\mathcal{V}_1(V_{11}) = \begin{pmatrix} V_{11} & 1 & 0 \\ 2 & 5 & 0 \\ 0 & 1 & -5 - V_{11} \end{pmatrix}$$

- The eigenvalues and eigenvectors are given as:

$$\lambda_{V1} = 0.5(5 + V_{11} - \sqrt{33 - 10V_{11} + V_{11}^2}) \quad \lambda_{V2} = 0.5(5 + V_{11} + \sqrt{33 - 10V_{11} + V_{11}^2}) \quad \lambda_{V3} = -5 - V_{11}$$

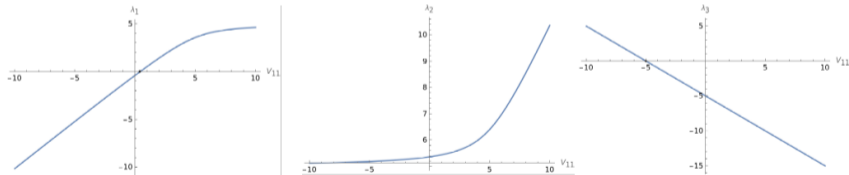


Figure: The parametric dependence of each eigenvalue on  $V_{11}$

- The velocity field is always a radial null.



# Example: Radial Null

- Case 1:  $V_{11} < -5$ .
  - $\lambda_{V_1} < 0$ ,  $\lambda_{V_2} > 0$ ,  $\lambda_{V_3} > 0$ .
  - Spine lies along  $\xi_1$  : Stable subspace.

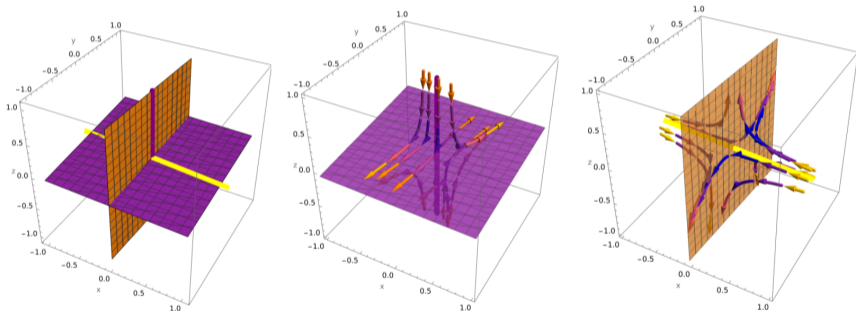


Figure: (a) Orientation of Separatrices, (b) Structure of  $\mathbf{B}$  and (c) Structure of  $\mathbf{v}$

- Case 2:  $V_{11} = -5$ . Degenerate case.

# Example: Radial Null

- Case 3:  $-5 < V_{11} < 0.4$ .
  - $\lambda_{V_1} < 0$ ,  $\lambda_{V_2} > 0$ ,  $\lambda_{V_3} < 0$ .
  - Spine lies along  $\xi_2$  : Unstable subspace.

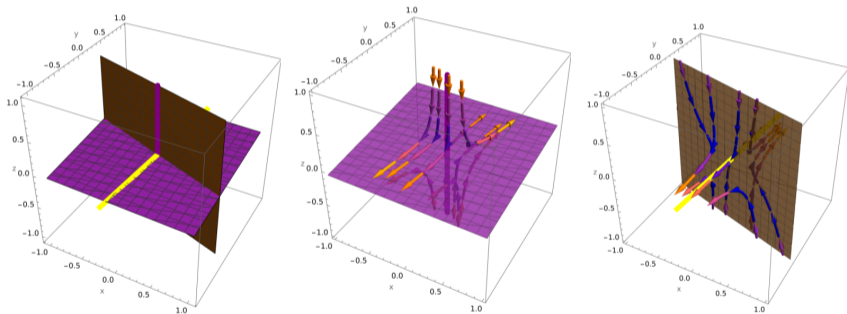


Figure: (a) Orientation of Separatrices, (b) Structure of  $\mathbf{B}$  and (c) Structure of  $\mathbf{v}$

- Case 4:  $V_{11} = 0.4$ . Degenerate case.

# Example: Radial Null

- Case 5:  $V_{11} > 0.4$ . Spine lies along  $\xi_3$  : Stable subspace.
  - $\lambda_{V_1} > 0, \lambda_{V_2} > 0, \lambda_{V_3} < 0$
  - Spine lies along  $\xi_3$  : Stable subspace.

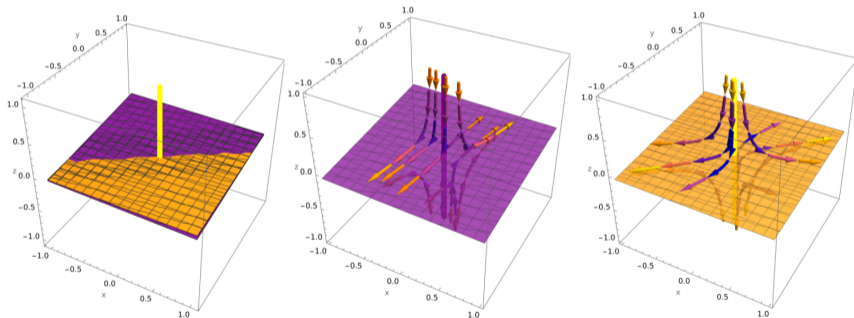


Figure: (a) Orientation of Separatrices, (b) Structure of  $\mathbf{B}$  and (c) Structure of  $\mathbf{v}$

## Spiral structure for $\mathbf{v}$ ?

- The characteristic polynomial of  $\mathcal{V}_1(V_{11}, b, q, j_{\parallel}, j_{\perp})$  can be written in the following form:

$$\left(x^2 - (\lambda_1 + \lambda_2)x + \lambda_1\lambda_2\right) (x - \lambda_3) = 0$$

- For the roots to be complex, the discriminant must be negative.

$$\frac{3j_{\parallel}(1+b) + q(-1+b) - S}{6j_{\parallel}} < V_{11} < \frac{3j_{\parallel}(1+b) + q(-1+b) + S}{6j_{\parallel}}$$

where  $S = (3j_{\parallel} + q)\sqrt{j_{\parallel}^2 - q^2}$

- The condition for existence of spiral nulls

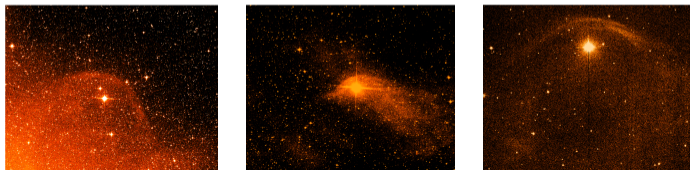
$$j_{\parallel} > |q| \quad \text{or} \quad j_{\parallel} < -|q|$$

# Future Work

- The estimate of pressure, along with the characteristic values of density, can give us the emission measure in say  $H\alpha$  (e.g. Rybicki and Lightman, 1979).

$$EM \propto \text{coeff. of transition}(T_e) \times n_e^2 \approx T_e n_e^2$$

- 3D MHD simulations to compute synthetic skymaps and estimate the emission.
- Comparison with observations. (Our  $H\alpha$  survey on BSG bow shock structures)



# Conclusions

- The linearized equations of resistive MHD were solved analytically in a local region close to the null point where both velocity field and magnetic field are zero.
- The solutions can be described in terms of the magnetic field parameters, and two free parameters.
- As the next step, we would like to find a better method of categorize the solutions.
- Emission measure can be calculated by estimating the pressure, density, and hence temperature. This can be then compared to the results from simulations and observations.